

## Low I<sub>Q</sub> Powering Solutions for One Alkaline Battery

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### INTRODUCTION

Designing single cell battery-powered applications requires good knowledge and understanding of the battery's capabilities and its chemistry as well as choosing the optimum converter to power the target application.

This application note focuses on the efficient utilization of alkaline cells, considering safety precautions provided by battery manufacturers and recommending the appropriate circuitry and converter topology for low-voltage applications that are powered from a single cell.

### ALKALINE BATTERY CONSIDERATIONS WHILE POWERING BOOST CONVERTERS

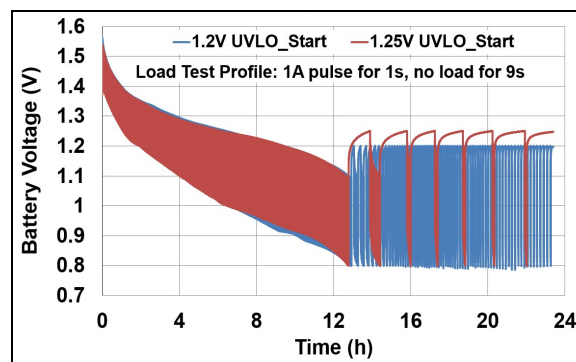
Battery manufacturers (OEMs) do not recommend the utilization of a battery below its specified Functional End Point (FEP) or cut-off voltage. This is a battery voltage value where there is not enough energy to deliver power as "all usable capacity" is used up. For an alkaline cell, the FEP is 0.9V or 0.8V. Discharging below the FEP even with a very small current will increase the risk of the battery to leak.

Leaking may produce serious damage (mostly irreversible) to the applications or the battery casing. Figure 1 shows a battery some time after it leaked. Corrosion can be noticed.



**FIGURE 1:** Discharged Alkaline Battery after Leakage, Showing Corrosion (Left Side).

As the battery discharges, its energy capacity decreases while its internal electrical resistance increases. A notable difference (hundreds of millivolts) can be observed between the open load and the loaded battery's voltage due to the internal resistance. As expected, this voltage drop is dependent upon the load's current flow.

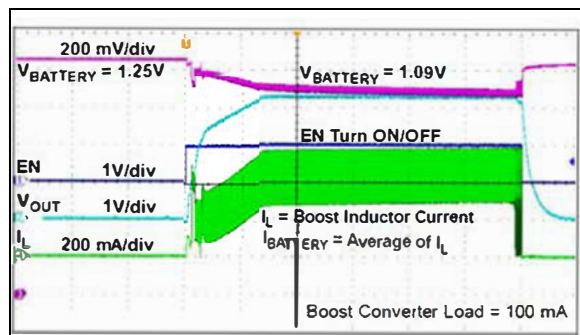


**FIGURE 2:** AA Alkaline Cell Discharged with Two Simulated UVLO Start Thresholds at 1.2V and 1.25V Using a Pulsed Load Profile. FEP is Set to 0.8V.

When the load is removed, the battery voltage starts to recover slowly, in a matter of minutes. This process may bring the battery voltage close to its nominal value. However, a nearly depleted battery will not be capable of maintaining its voltage once the load is applied again because of its increased internal resistance. This will result in a bigger voltage drop which will impact the proper start-up of the DC-DC converter. This malfunction can affect time-variable load applications such as personal care products, wireless transmitters/receivers, data loggers, etc. The experiments illustrated in Figure 2 and Figure 3 demonstrate this issue. Fresh AA alkaline batteries are discharged down to 0.8V with the following profile: cycles of 1A load for 1 second followed by cycles of no load for 9 seconds. As shown in Figure 2, the battery voltage drop is the result of the increase of the battery's internal resistance from approximately 100 mΩ to approximately 300 mΩ (battery's voltage drop divided by load current). Usually, when an alkaline battery reaches its FEP (0.8V), its internal resistance increases up to 800 mΩ. For the purpose of this demonstration, two virtual UVLO Start thresholds were generated to simulate two real DC-DC start-up scenarios: 1.2V and 1.25V. Figure 2 illustrates that, after being discharged to the approximate 0.8V limit, the battery recovers slowly and

cannot ensure proper start-up or functioning under the 1A load. As the load applied to the battery through the DC-DC converter increases, the higher the UVLO Start threshold and the better the protection for the system.

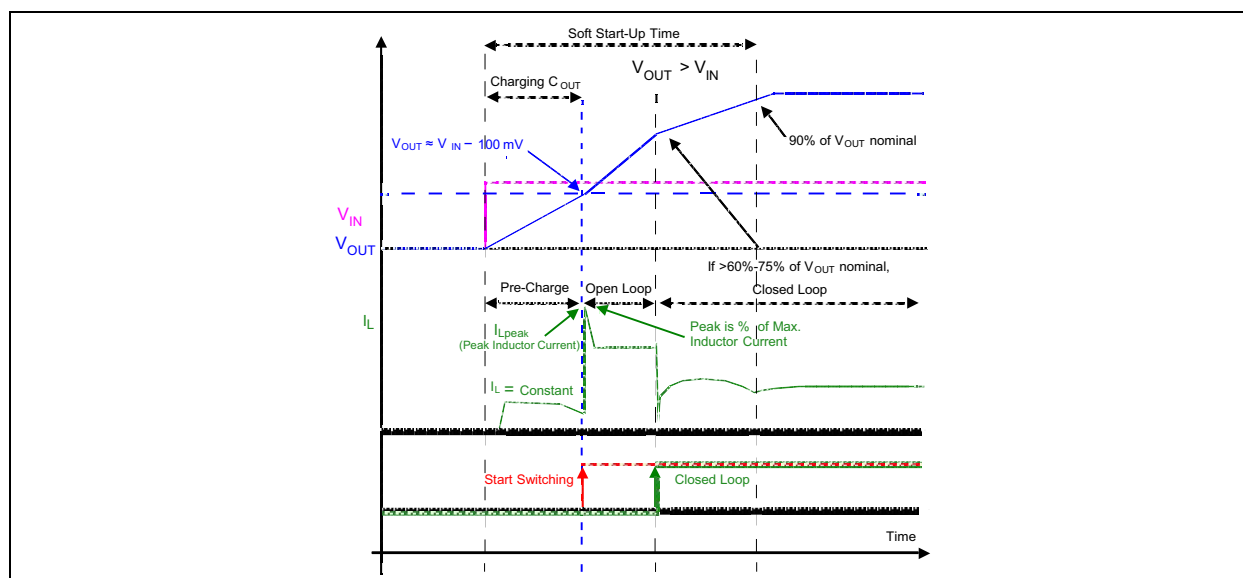
Therefore, the UVLO Start threshold must be well correlated with the load current. In the case of step-up (boost) converters, their peak inductor current limit,  $I_{Lpeak}$  (see Table 1) or the current consumed from the battery (equal with the average of the inductor's current) is a few times higher than what the application's load consumes.



**FIGURE 3:** A Start-Up Example with an In-Use Battery Showing an Approximate  $0.38\Omega$  Internal Resistance. (Notice the Voltage Drop from 1.25V to 1.09V while Load Is Powered.)

For step-down (buck) converters, the battery current is lower than the load current. However, there are rare cases or applications for which a single battery voltage needs to be lowered. Therefore, the focus is on boost converters as they are more critical when choosing the input power. All boost converters require a larger amount of energy during their start-up sequence, a high peak current for a short period, usually hundreds of milliamps for tens of microseconds. A typical start-up sequence for a boost converter is shown in Figure 4.

A low voltage synchronous boost DC-DC start-up sequence begins with a linear, constant charge of the output capacitor using a controlled current. The synchronous rectifier works in the linear (or ohmic) region and the amount of load current is gate controlled. This part is called the "Pre-Charge" phase of the output capacitor and tracks the output to reach the battery's value (minus a small drop of hundreds of millivolts on the rectifier switch). Then, the device starts switching in "Open Loop" mode with limited inductor peak current. This current is usually a percentage of the maximum peak inductor current. When the output voltage reaches more than 60%-75% of its target, the converter's logic switches in "Closed Loop" PWM mode and starts regulating. Therefore, the "Pre-Charge" and "Open Loop" phases require a large amount of energy for very small periods to ensure proper start-up and to reach the nominal output voltage set.



**FIGURE 4:** Microchip Boost Converters Typical Start-Up Sequence.

As the discharged battery is not able to provide the necessary energy, a converter without any start-up protection circuit such as "UVLO Start" or "UVLO Stop" may end up in a loop in which it attempts to start unsuccessfully. At each attempt, it drains a large amount of current, draining the battery even more.

There are a number of step-up converters designed with very low cut-off voltage, down to 0.35V-0.5V. Even though a battery boost circuit might be able to operate

down to a very low input voltage, discharging alkaline cells below 0.8V is not advisable. Below 0.8V, parasitic drains should be kept as low as possible and preferably removed entirely. N.B.: *There are exceptions to this: some OEMs recommend that alkaline cells be discharged down to 0.5V if the cell's voltage is strictly monitored.*

Operating temperature may also impact device performance. Cold environments, in particular, may reduce runtime. Extremely high temperatures can also cause serious damage. Engineers should consider this aspect and always correlate battery temperature operating ratings and the environment in which their application will be used.

## MICROCHIP ONE CELL-POWERED DEVICES SOLUTIONS OVERVIEW

The Microchip one-cell converters enable designers to use a wide variety of battery types to power applications that generally require higher operating voltages. [Table 1](#) summarizes Microchip low-voltage, single cell-powered management devices. One of these devices, the MIC23099, is a power management IC (PMIC) that offers both boost and buck capabilities.

The MCP1640 is the best known and first designed step-up (boost) solution in the family, a high-performance low-voltage boost converter with only 19  $\mu\text{A}$  quiescent current and 800 mA peak input current limit. The MCP1623/4 are low-cost versions of the MCP1640 that provide half peak current limit, less output current and a  $\pm 7\%$  output voltage accuracy. With 650 mA  $I_L$  peak limit, the MCP16251/2 is the best in the family, offering the lowest quiescent current ( $I_Q$ ) for energy saving, with only 4–5  $\mu\text{A}$  typical. The  $I_Q$  bias for internal circuits comes from the output of the converter (after start-up), increasing the efficiency of the conversion. The MCP1642 offers 1.8A high inductor peak current. Its LED driver version, the MCP1643, provides an efficient solution for driving a power LED in constant current from one single alkaline cell.

It is to be noted that many of these power management solutions run on battery at very low voltage (e.g. 0.35V), after start-up (see [Table 1](#)).

**TABLE 1: LOW  $I_Q$ , ONE CELL-POWERED DEVICES OVERVIEW**

Device	$I_Q^3$ [ $\mu\text{A}$ ]	$V_{IN}$ [V]	$V_{OUT}$ [V]	$V_{Start-Up}$ [V]	$I_{Lpeak}$ [A]	$I_{Pre-Charge}^4$ [mA]	$I_L$ Open Loop <sup>4</sup> [mA]	Features
MIC23099 <sup>1</sup>	—	0.5-1.6	1.0-3.3	0.75	1.5	80	120	Boost and Buck Mode, Power Good and Low Battery Monitoring
MCP16251/2	4	0.35-5.5	1.8-5.5	0.82	0.65	130	550	PFM/PWM, True Disconnect Output or Input-to-Output Bypass
MCP1640/B/C/D	19	0.35-5.5	2.0-5.5	0.65	0.8	130	—	PFM/PWM or PWM Only, True Disconnect Output or Input-to-Output Bypass
MCP1623/4	—	0.35-5.0	2.0-5.5	0.65	0.425	130	—	PWM/PFM Mode or PWM Mode Only
MCP1642B/D	400	0.35-5.5	1.8-5.5	0.65	1.8	200	1100	Power Good, PWM, True Disconnect Output or Input-to-Output Bypass
MCP1643 <sup>2</sup>	—	0.5-5.0	max. 5.0	0.65	1.6	—	—	Open Load Protection (output overvoltage)

**Note 1:** MIC23099 is a dual output Boost and Buck converter.  $I_{Q\_PFM}$  is 200  $\mu\text{A}$  typical in the following conditions: no load on both outputs, device is running (switching) and the LED pin is not connected.

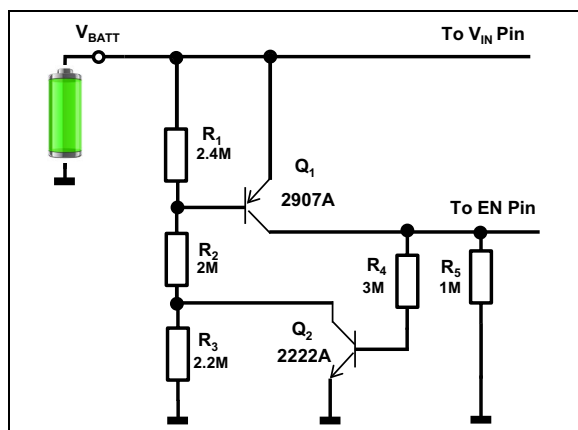
**2:** MCP1643 is an LED Constant Current Regulator. If no LED is connected,  $V_{OUT}$  will be clamped at 5V maximum. Minimum LED current to achieve regulation is approximately 15 mA for one alkaline cell. While in shutdown, the device consumes 1.2  $\mu\text{A}$  typical.

**3:**  $I_Q$  is in sleep mode — device is not switching. This is the current necessary to bias the device's internal blocks and is measured at  $V_{OUT}$ .

**4:** Values are from bench testing on a limited number of samples, not characterized values. The Pre-Charge and  $I_L$  Open Loop currents were measured for  $V_{OUT} = 3.3\text{V}$  and  $V_{IN} = 1.25\text{V}$  with 1 mA load at room temperature.

These devices have been designed to operate with a wide input voltage range, starting from 0.65V-0.82V and running down to 0.35V, with the purpose of accommodating a large variety of input sources (battery types). For alkaline batteries in particular, if the application has no other control circuits for monitoring the battery's voltage (a system microcontroller), there might be a need for a simple and inexpensive analog discrete UVLO Start/Stop circuit with ultra-low additional power consumption, as shown in Figure 5. This circuit is powered from the same input source or battery and consumes only 0.5  $\mu$ A-2  $\mu$ A (Figure 6). Also, it can easily drive the Enable (EN) pin of the boost converter and both "Start" and "Stop" thresholds are user programmable using Equation 1 and Equation 2.

The circuit in Figure 5 offers approx. 1.1V trip point to start and 0.8V to shut down.



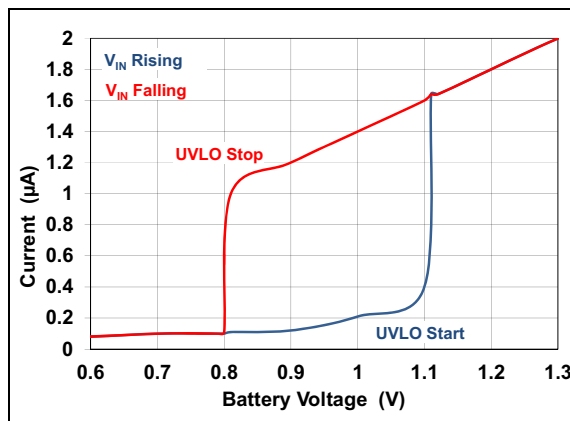
**FIGURE 5:** Ultra-Low  $I_Q$  UVLO Circuit Example, with 1.1V Start-Up and 0.8V Shutdown Thresholds.

## EQUATION 1:

$$UVLO V_{IN\_START} \approx 0.4 \times \frac{R_1 + R_2 + R_3}{R_1}$$

## EQUATION 2:

$$UVLO V_{IN\_STOP} \approx 0.4 \times \frac{R_1 + R_2}{R_1}$$



**FIGURE 6:** Current Consumed by the Additional UVLO Circuit in Figure 5.

**Note:** For the evaluation of the UVLO circuit in Figure 5, the following reference design is available on the Microchip website:

- MCP16251 Reference Design – ARD00797

## MIC23099 — BOOST AND BUCK PMIC WITH BATTERY MONITORING

The MIC23099 is a One-Cell Power Management Controller (PMIC) which integrates one boost and one low current buck converter. The buck section is powered internally directly from the boost's output and can supply up to maximum 30 mA to the load, being one of the very few low-power, under 2V input step-down solutions on the market. It can convert the 1.8V input or the battery's voltage down to 0.9V.

The MIC23099 features a battery monitoring circuit. An open drain output can provide information on the battery status to any system's MCU. The LED output pin shows the battery level is low. While the battery gets discharged and reaches the device's internal 1.2V threshold, the LED will start blinking at low intervals (0.25 Hz and 25% duty cycle), until the user replaces the battery.

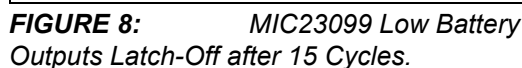


## CONCLUSION

Engineers should avoid deeply discharging alkaline batteries because it will increase the possibility of leakage. Even though a boost DC-DC converter might be able to operate down to a very low input voltage, discharging alkaline batteries below 0.8V is not advisable. Below 0.8V on the battery, parasitic drains should be kept as low as possible and preferably removed entirely. Alkaline batteries can be discharged down to 0.5V if the cell voltage is well monitored using dedicated circuits.

## REFERENCES

1. MIC23099 Data Sheet – “Single AA/AAA Cell Step-up/Step-Down Regulators with Battery Monitoring” (DS20005684)
2. MCP16251/2 Data Sheet – “Low Quiescent Current, PFM/PWM Synchronous Boost Regulator with True Output Disconnect or Input/Output Bypass Option” (DS20005173)
3. MCP16251 Reference Design – “One-Cell Boost Converter with External UVLO Circuit” (DS50002561)
4. MCP1640/B/C/D Data Sheet – “0.65V Start-Up Synchronous Boost Regulator with True Output Disconnect or Input/Output Bypass Option” (DS20002234)
5. MCP1623/4 Data Sheet – “Low-Voltage Input Boost Regulator for PIC<sup>®</sup> Microcontrollers” (DS40001420)
6. MCP1642B/D Data Sheet – “1.8A Input Current Switch, 1 MHz Low-Voltage Start-Up Synchronous Boost Regulator” (DS20005253)



7. MCP1643 Data Sheet – “1 MHz Low Start-up Voltage Synchronous Boost LED Constant Current Regulator” (DS20005208)
8. MIKROE-2765 – “MIC23099 Click Board - visit <https://www.mikroe.com/mic23099-click>

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